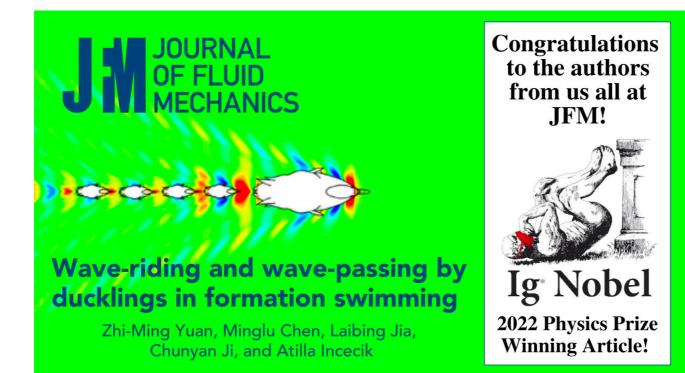
WAVE DRAG AND WAVE THRUST PHENOMENA

GRAHAM BENHAM SCHOOL OF MATHEMATICS AND STATISTICS UNIVERSITY COLLEGE DUBLIN IRELAND

DUCKS IN A ROW



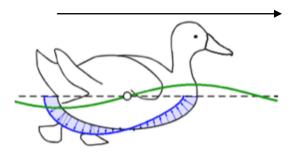
https://www.youtube.com/user/RobinEAdams



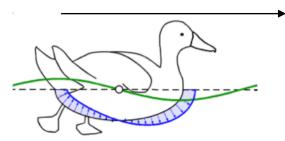
WAVE DRAG (WAKE)

WAVE THRUST (SURFING WAVES)

Poor positioning: Swimming **against** surface gradients



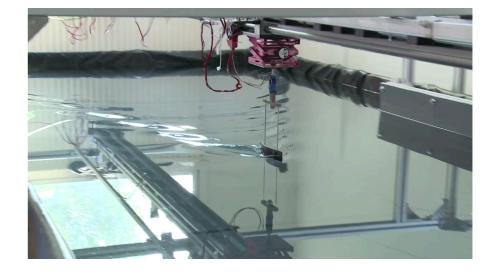
Good positioning: Swimming **with** surface gradients



LECTURE OUTLINE

WAVE DRAG PHENOMENA

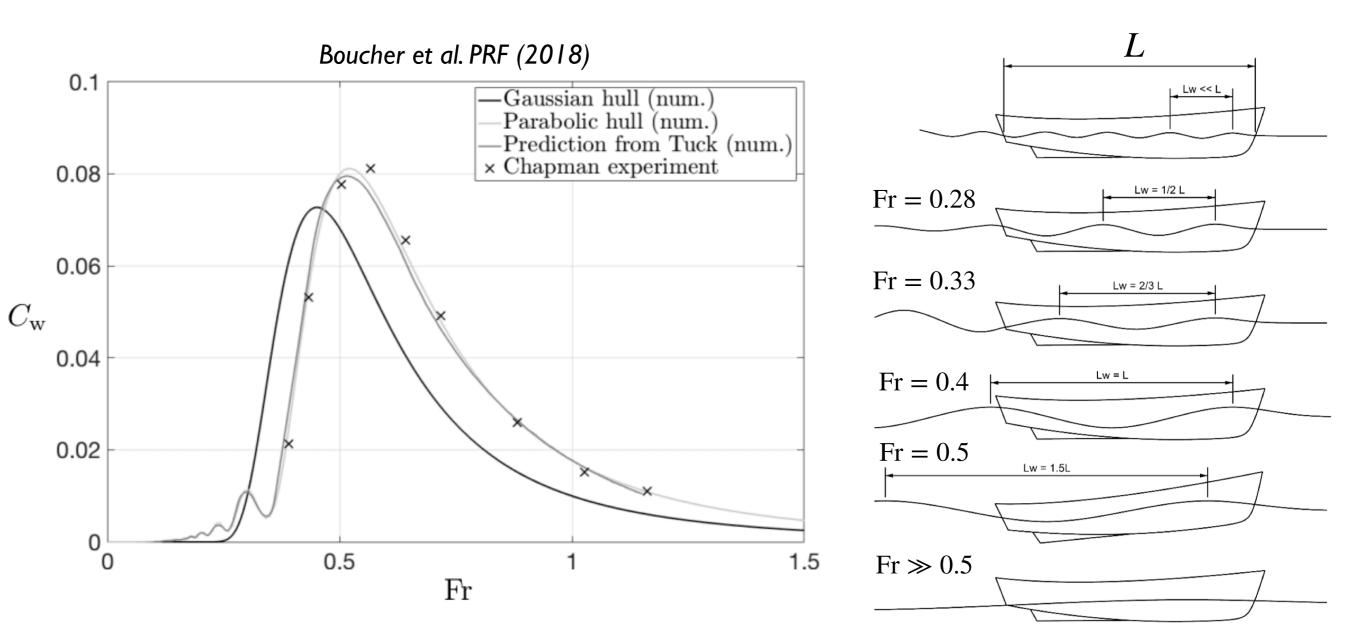
I. SHAPE OF OBJECT
 DEPTH OF WATER



WAVE THRUST PHENOMENA I. GUNWALE BOBBING 2. SURFERBOT



WAVE DRAG IN DEEP WATER

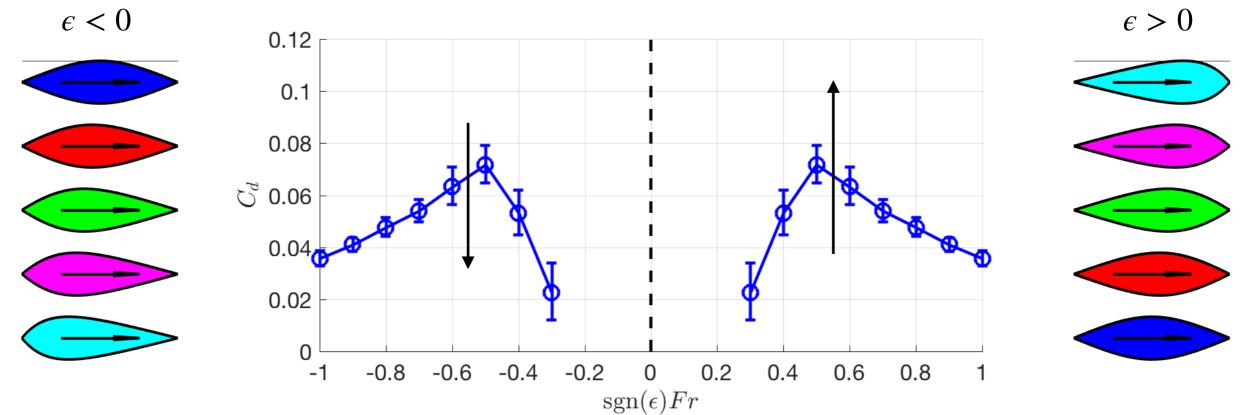


$$C_w = \text{Drag}/\rho U^2 L^2$$

Fr = U/\sqrt{gL}

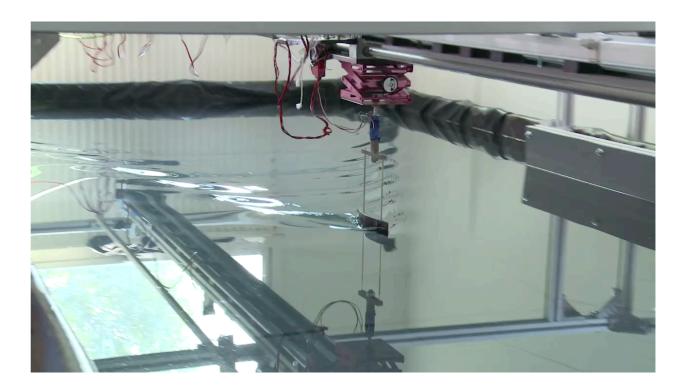
Resonance between boat length and wavelength

I. EFFECT OF SHAPE ASYMMETRY



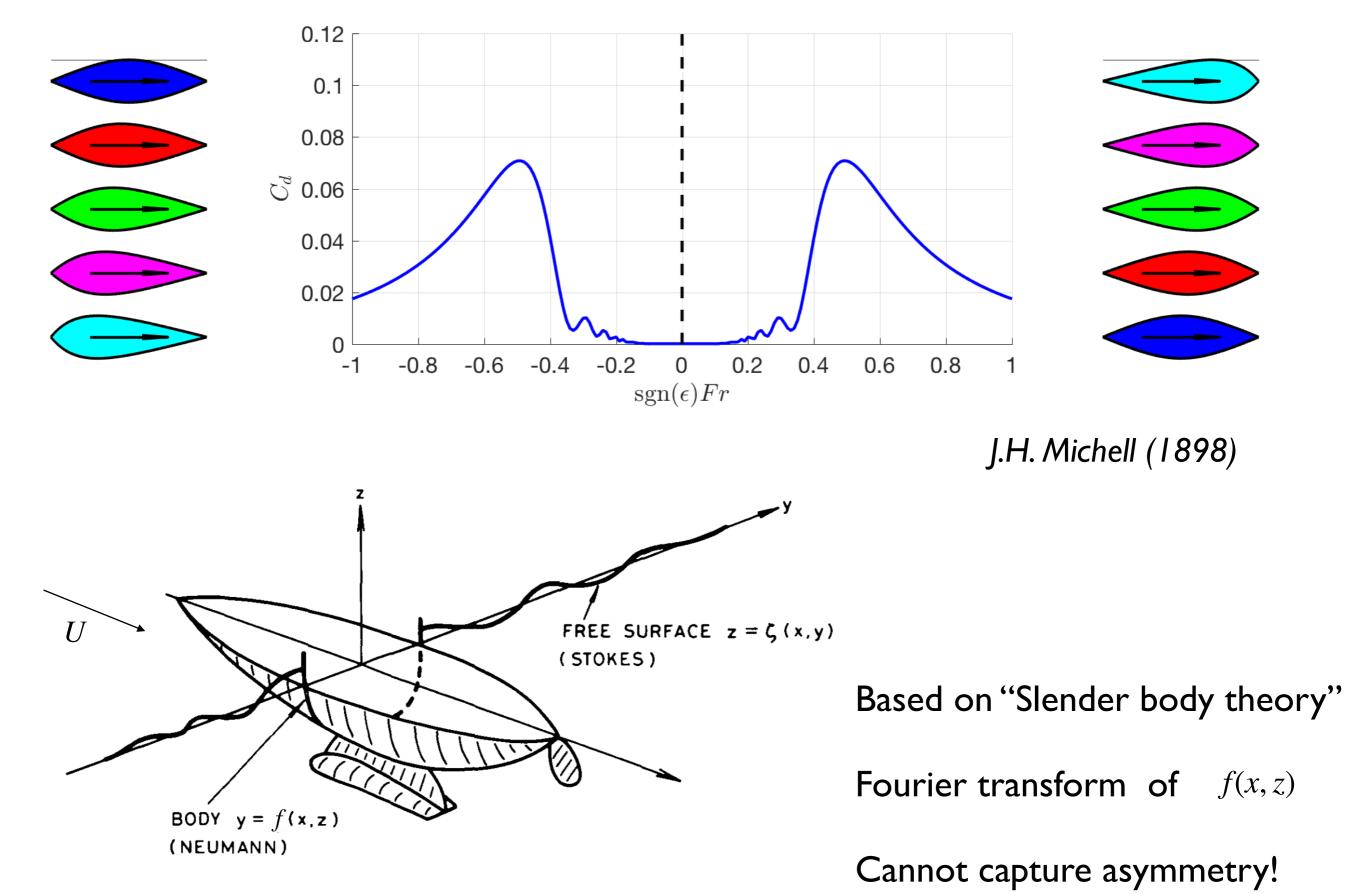
Parameterised family of curves





Tow tank with a force sensor

MICHELL'S THEORY FOR THE WAVE DRAG



SYMMETRY PARADOX

EULER EQUATIONS:

$$\nabla \cdot \boldsymbol{u} = \boldsymbol{0},$$
$$\rho(\boldsymbol{u} \cdot \nabla)\boldsymbol{u} = -\nabla p - \rho g \hat{\boldsymbol{k}}$$

$$v = \pm u f'(x)$$
, on $y = \pm f(x)$,

BOUNDARY CONDITIONS: $w = u\zeta_x + v\zeta_y$, on $z = \zeta(x, y)$, $p = p_{atm}$, on $z = \zeta(x, y)$,

$$\boldsymbol{u} \to (-U, 0, 0), \quad x, y, z \to \pm \infty,$$

APPLY THE TRANSFORMATION:

 $U \rightarrow -U, \quad \mathbf{u} \rightarrow -\mathbf{u}$

SYMMETRY PARADOX

EULER EQUATIONS:

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \rho (\mathbf{u} \cdot \nabla) \mathbf{u} = -\nabla p - \rho g \hat{k} + \mu \nabla^2 \mathbf{u}$$

$$v = \pm u f'(x)$$
, on $y = \pm f(x)$,

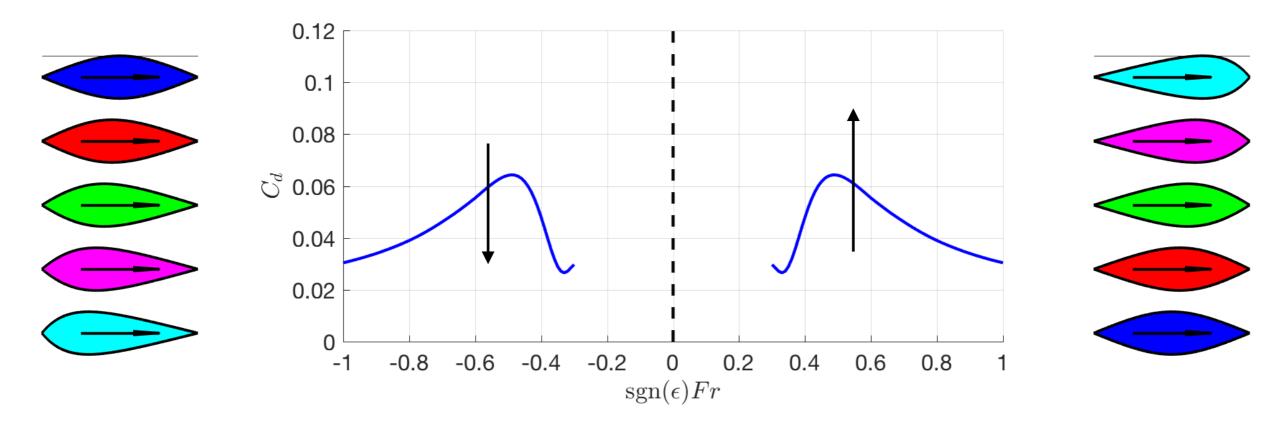
BOUNDARY
CONDITIONS:
$$w = u\zeta_x + v\zeta_y$$
, on $z = \zeta(x, y)$,
 $p = p_{atm}$, on $z = \zeta(x, y)$,

$$\boldsymbol{u} \to (-U, 0, 0), \quad x, y, z \to \pm \infty,$$

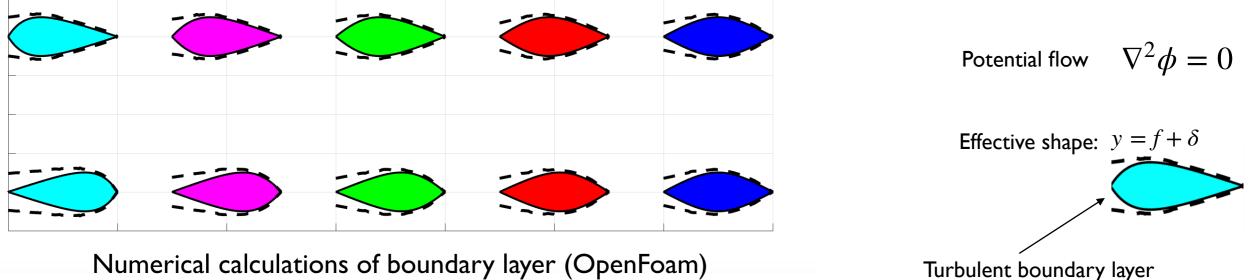
APPLY THE TRANSFORMATION:

$$U \rightarrow -U, \quad \mathbf{u} \rightarrow -\mathbf{u}$$

MODIFIED MICHELL'S THEORY

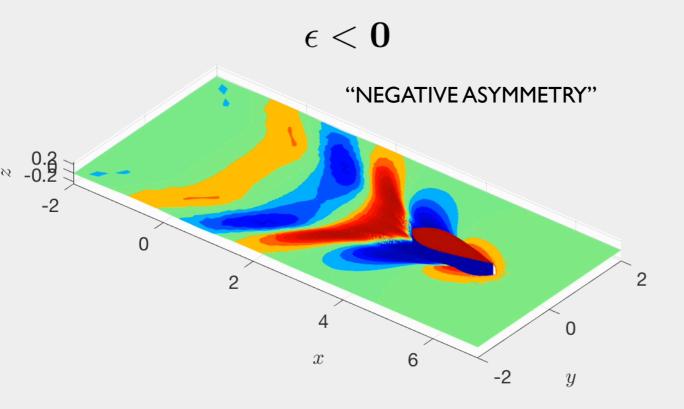


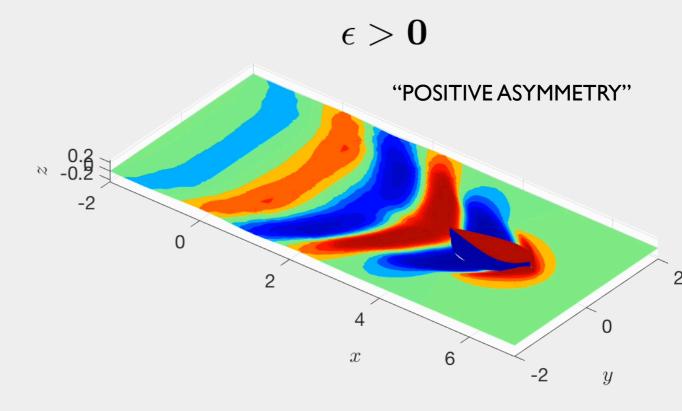
Effective shape: Hull + Boundary layer

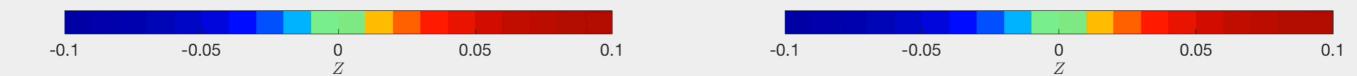


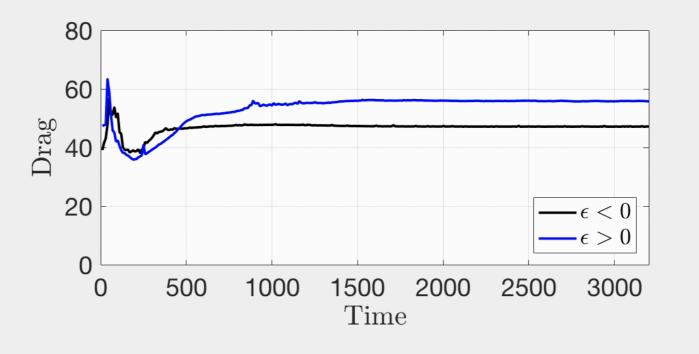
Turbulent boundary layer

OPENFOAM SIMULATIONS









GPB et al., JFM (2019)

2. EFFECT OF WATER DEPTH

Rodrigo de Freitas Lagoon, Rio de Janeiro, Brazil

Mean depth: 2.8 m, Maximum depth: 4.3 m



Lake Bled, Slovenia

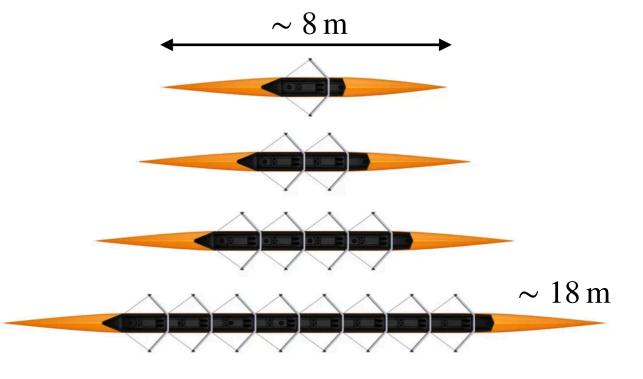
Maximum depth: 30 m, with a small island



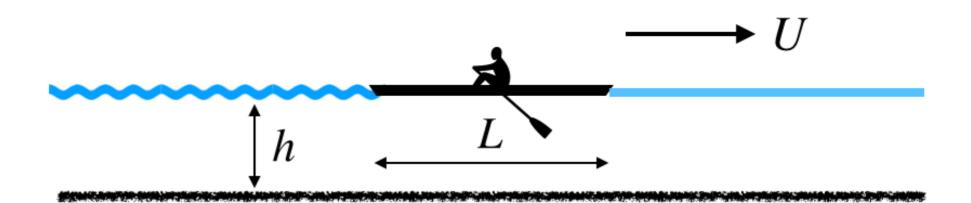
Sea forest waterway, Koto, Japan

Consistent depth: 6m

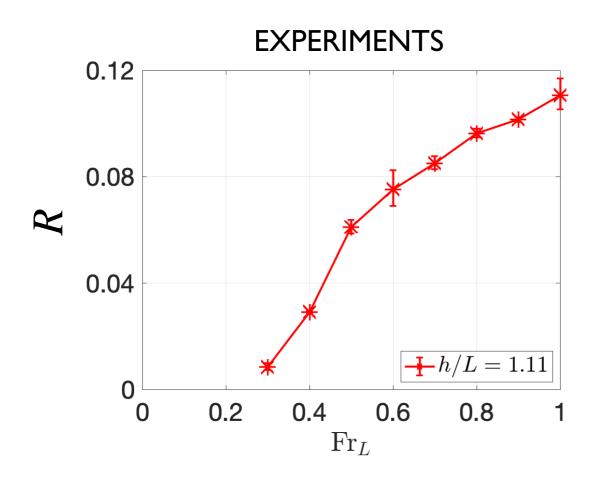








Rafid Bendimerad

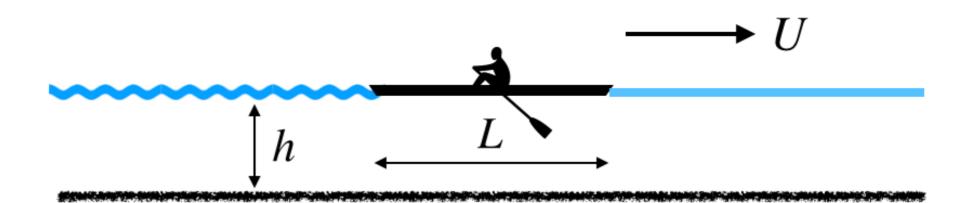


$$Fr_L = U/\sqrt{gL}$$
$$Fr_h = U/\sqrt{gh}$$

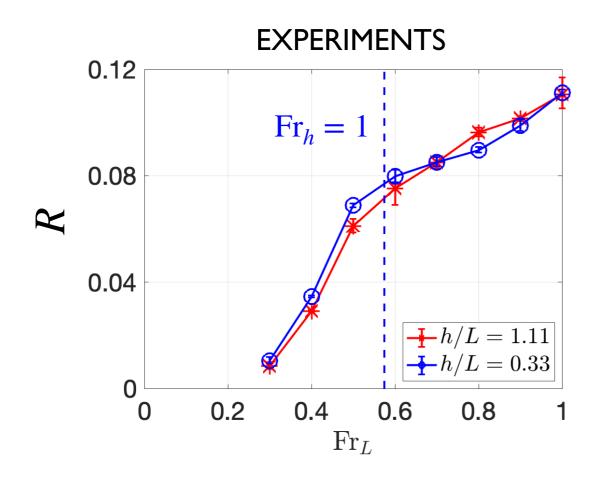
Normalisation:

$$R = \text{Drag}/\rho g L^3$$





Rafid Bendimerad

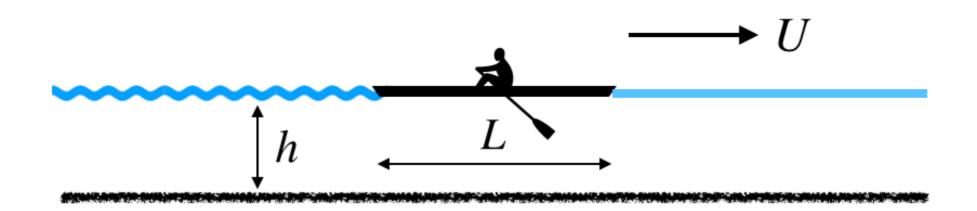


$$Fr_L = U/\sqrt{gL}$$
$$Fr_h = U/\sqrt{gh}$$

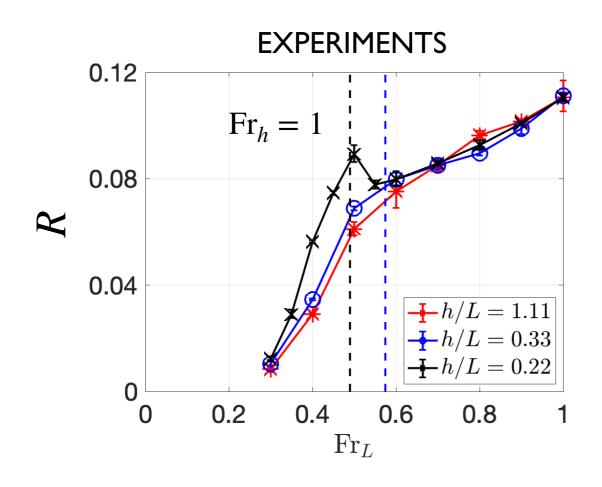
Normalisation:

$$R = \text{Drag}/\rho g L^3$$

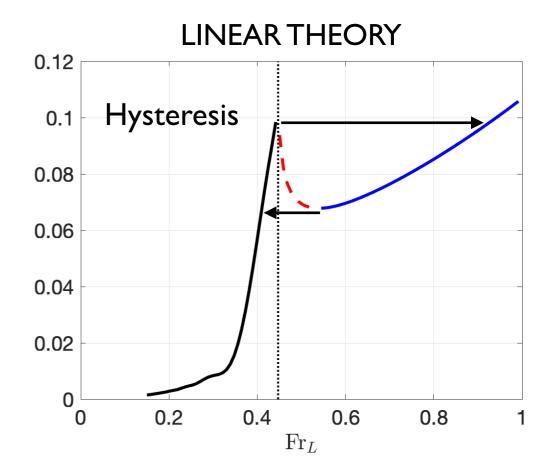




Rafid Bendimerad

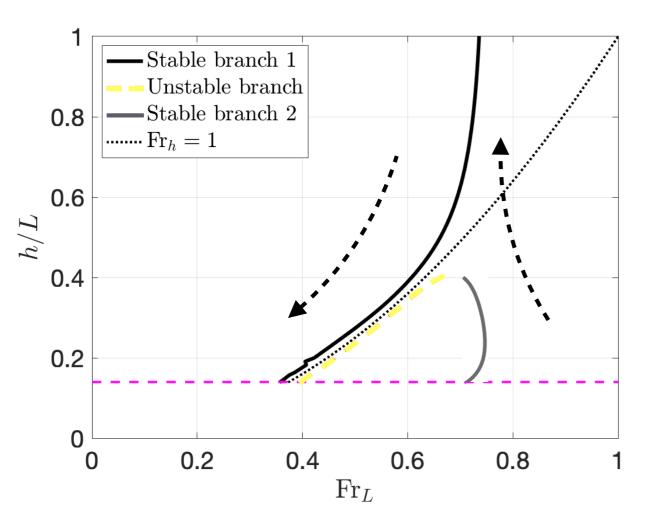


$$Fr_L = U/\sqrt{gL}$$
$$Fr_h = U/\sqrt{gh}$$

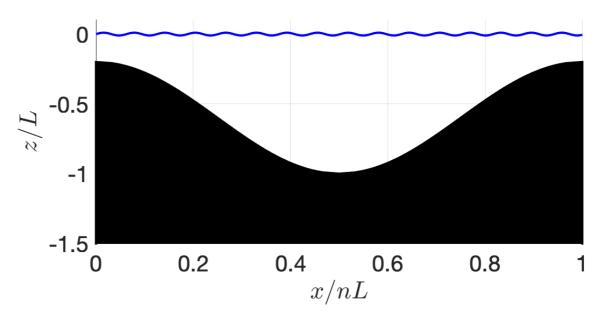


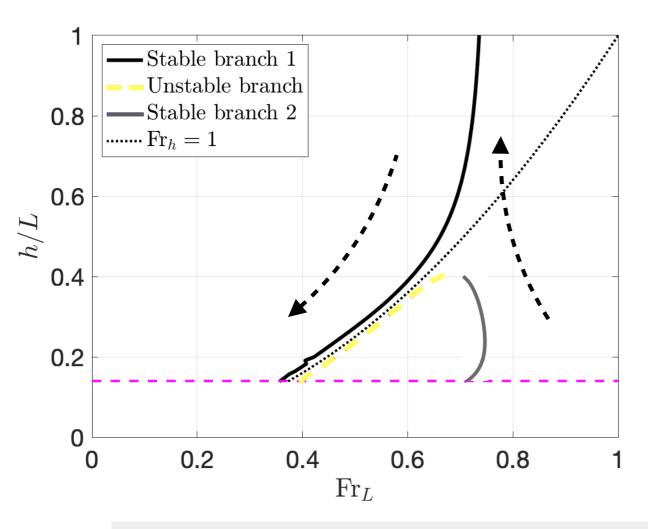
Normalisation:

 $R = \text{Drag}/\rho g L^3$

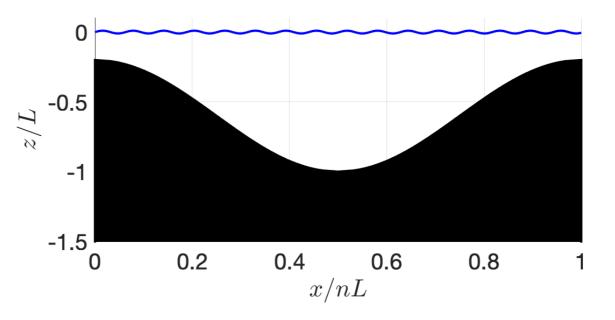


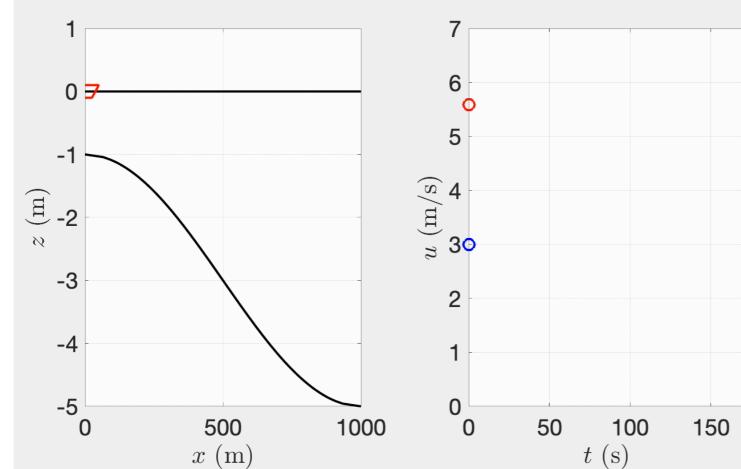
ROWING RACE WITH NON-UNIFORM WATER DEPTH

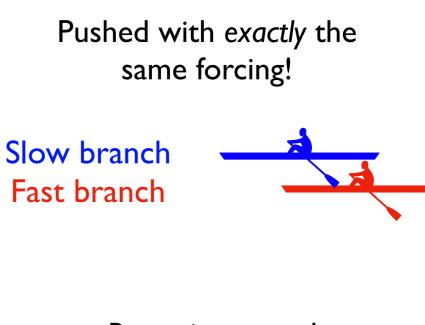




ROWING RACE WITH NON-UNIFORM WATER DEPTH







Race times can be improved by a few %

GPB, et al., PRF (2020)

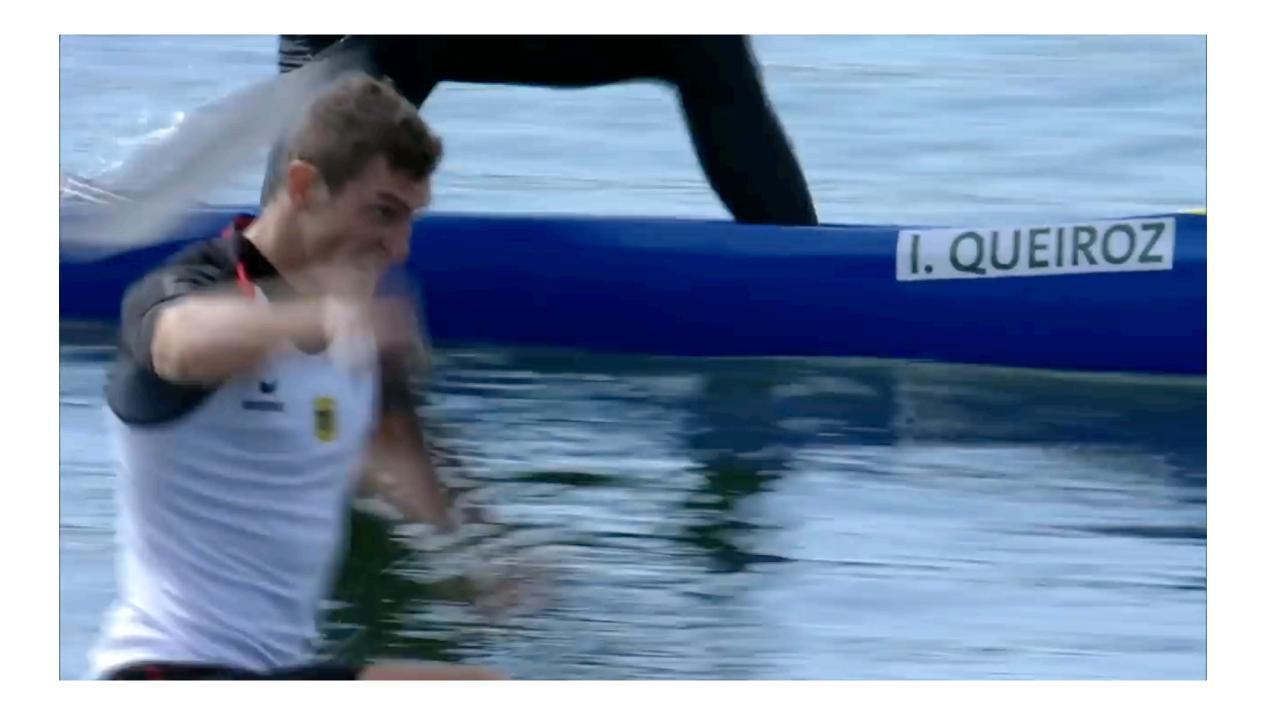
WAVE THRUST PHENOMENA



Jerome Neufeld Muldrew Lake, Ontario, Canada (August, 2021)

"GUNWALE BOBBING"

OLYMPIC CANOE SPRINT



Rio 2016 men's singles canoe 1000m



Amplitude: $A = 0.3 \,\mathrm{m}$ Frequency: $\nu \approx 0.5 \,\mathrm{Hz}$ Torso mass: $m \approx 20 \,\mathrm{kg}$

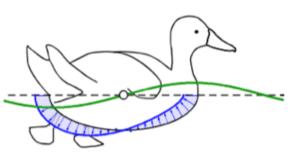
Vertical force: $F_V = m\ddot{z} = mA(2\pi\nu)^2 \approx 60 \text{ N}$ Horizontal force: $F_H \approx 300 \text{ N}$

20% of the force injected vertically!

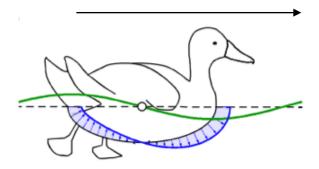
What is the impact on performance?

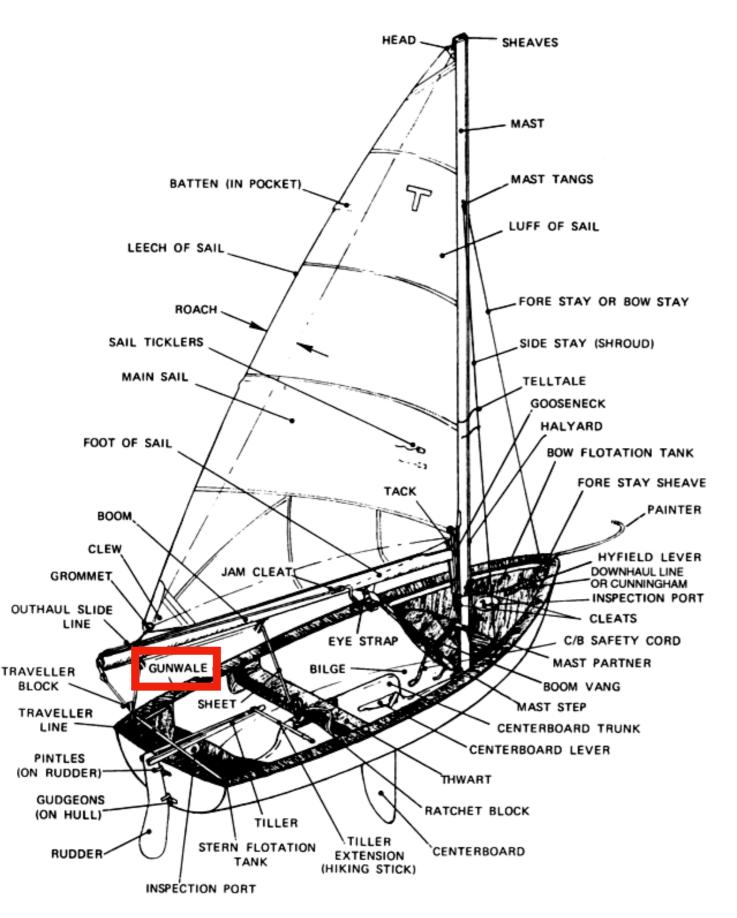
Can it be optimised?





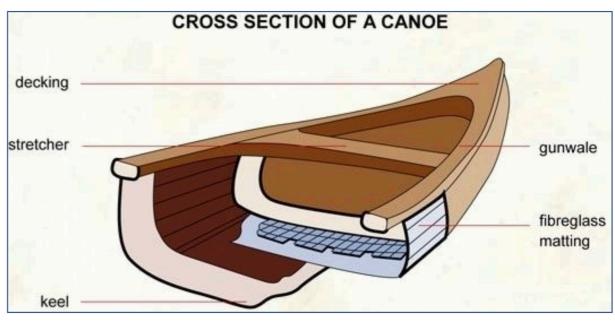
With surface gradients?





GUNWALE BOBBING

(pronounced gunnel)



gunwale
/ˈgʌn(ə)l/

noun

the upper edge or planking of the side of a boat or ship.

EXPERIMENTAL CAMPAIGN

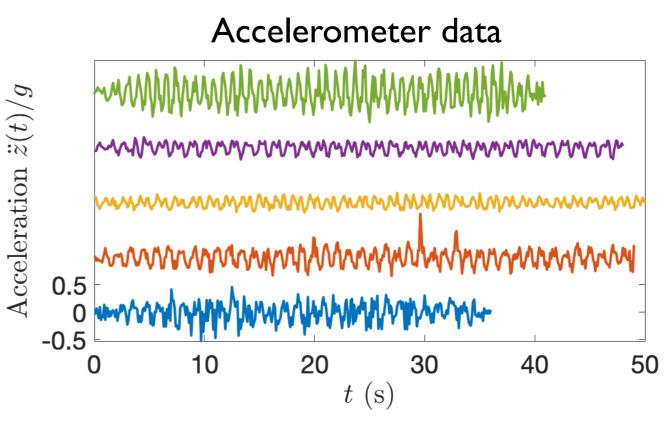
25 m



Ontario, Canada

Paddle-board: L = 3.05 mCanoe: L = 4.70 m Speed: U = 0.5 - 1.25 m/s

Frequency: $\nu = 1 - 1.5 \,\text{Hz}$



DEEP WATER WAVES

Wavenumber: $k = \omega^2/g$

Phase velocity:

$$c_p = \frac{\omega}{k} = \frac{g}{\omega}$$



DIMENSIONLESS PARAMETERS

Cruising Froude number: $Fr = \frac{U}{(gL)^{1/2}} \approx 0.14$ Oscillating Froude number: $Fr_{\omega} = \frac{c_p}{(gL)^{1/2}} \approx 0.19$

Mach number:
$$M = \frac{\mathrm{Fr}}{\mathrm{Fr}_{\omega}} = \frac{U}{c_p} \approx 0.73$$

Miles Neufeld, Paddleboard, Canada



Martin Digby, Canoe, YouTube



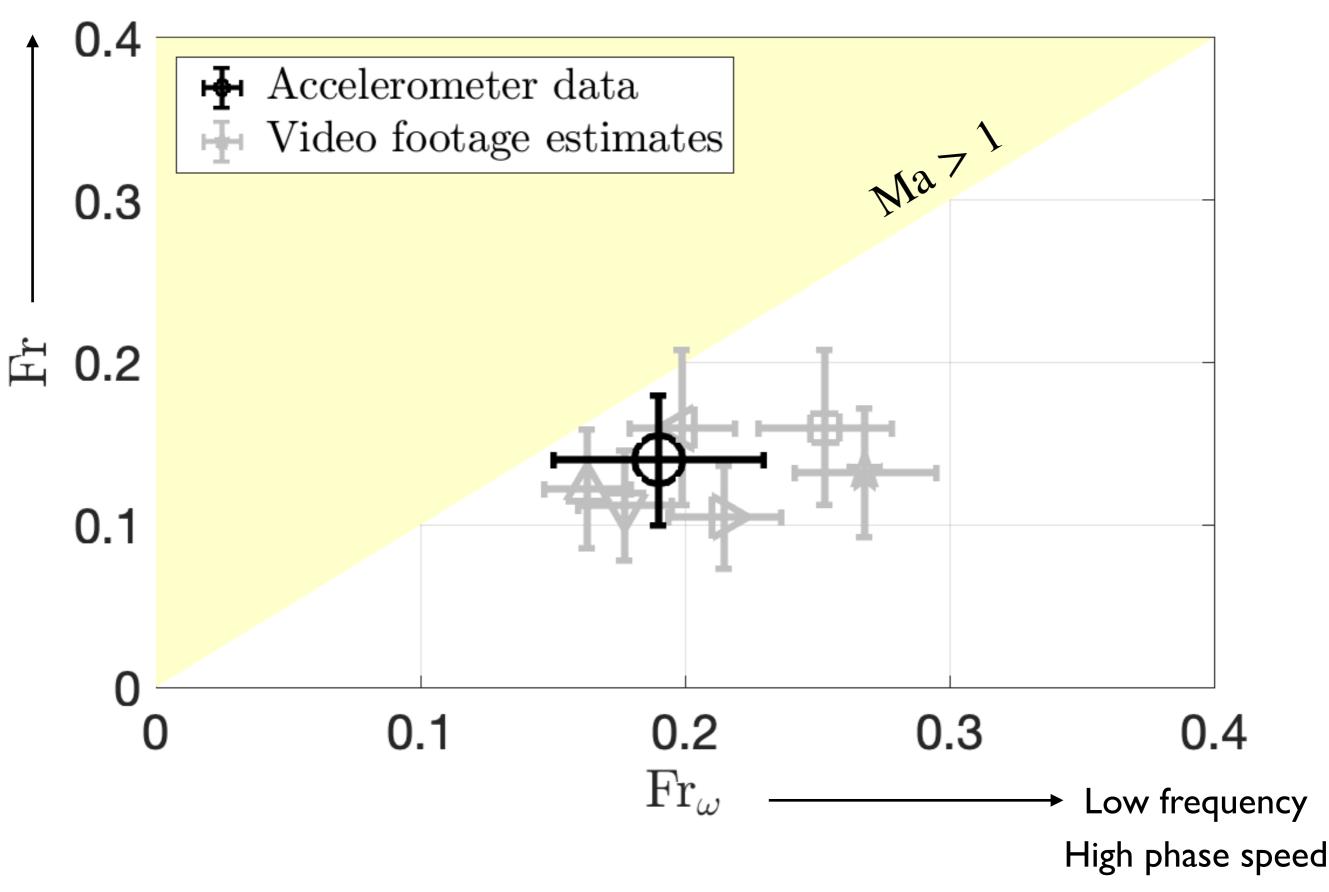
GPB, Punt, Oxford



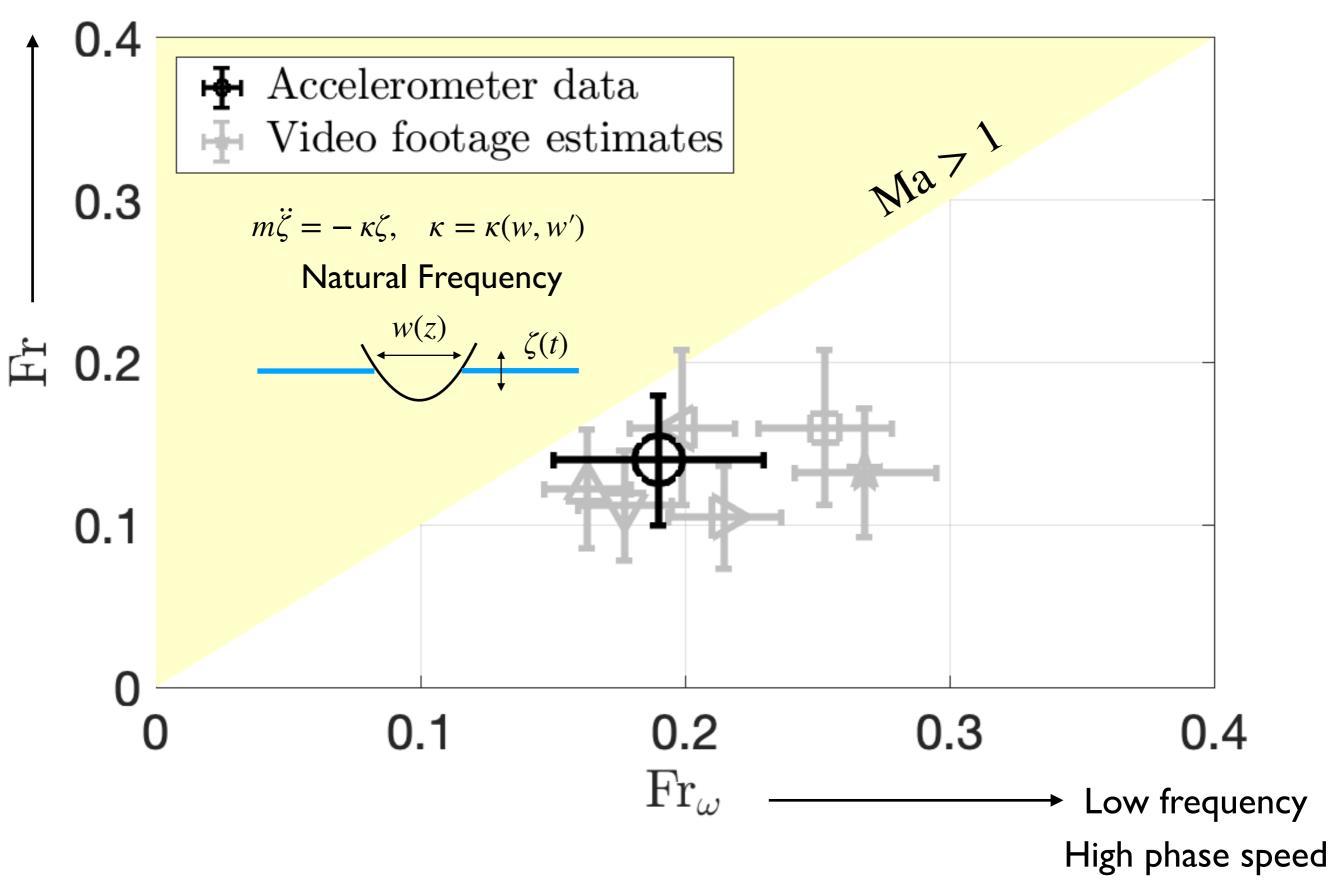
Jerome Neufeld, Canoe, Trinity College Cambridge

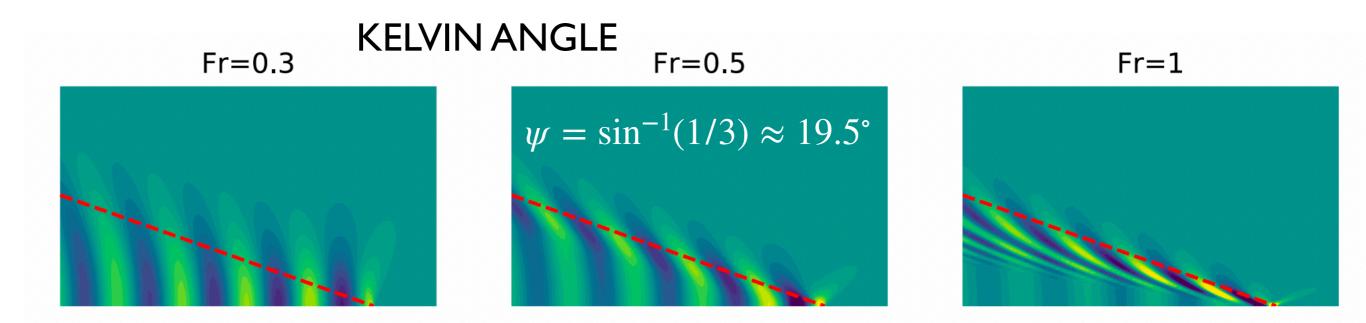


High speed

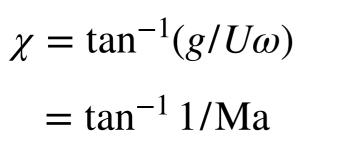


High speed





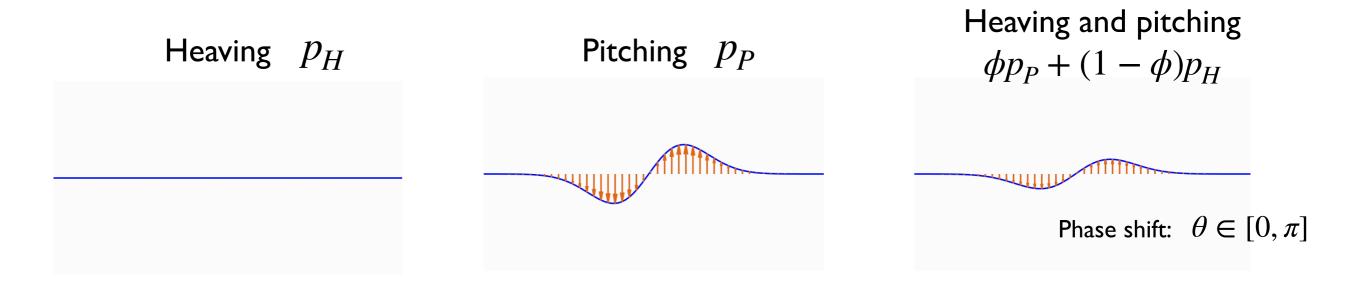
MACH ANGLE



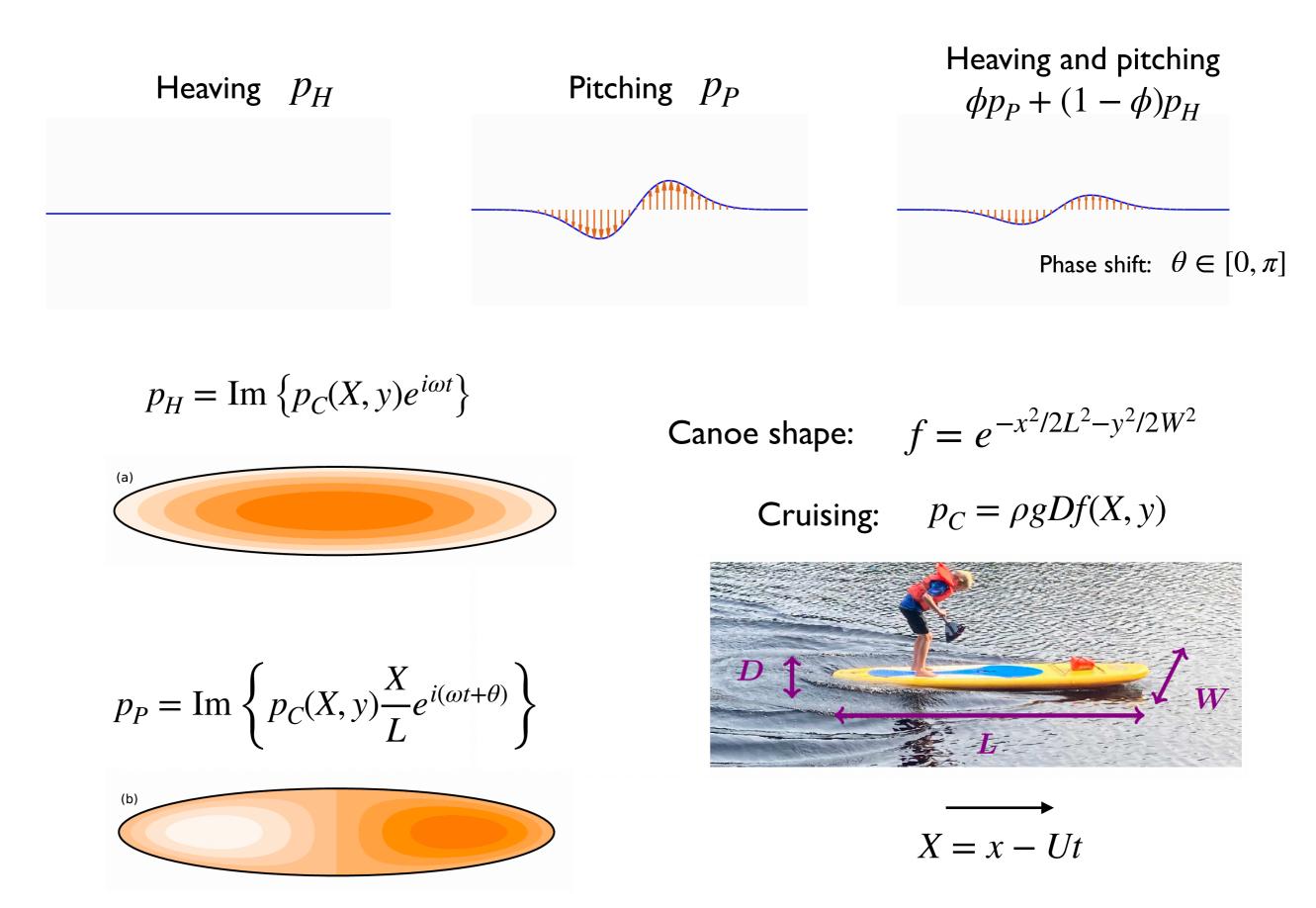
Waves due to bouncing (Mach) are **dominant** compared with waves due to cruising (Kelvin)

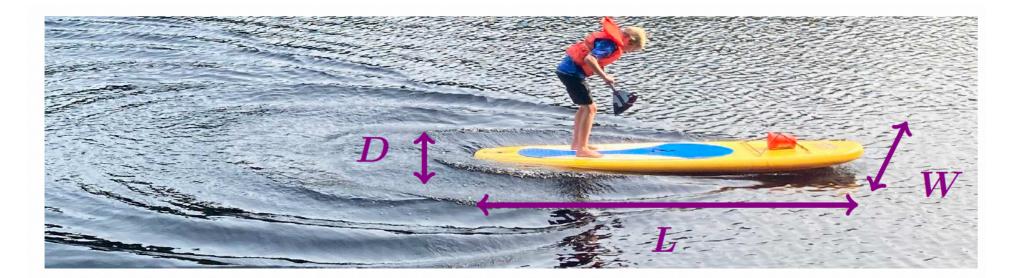


LINEAR MODEL FOR GUNWALE BOBBING



LINEAR MODEL FOR GUNWALE BOBBING

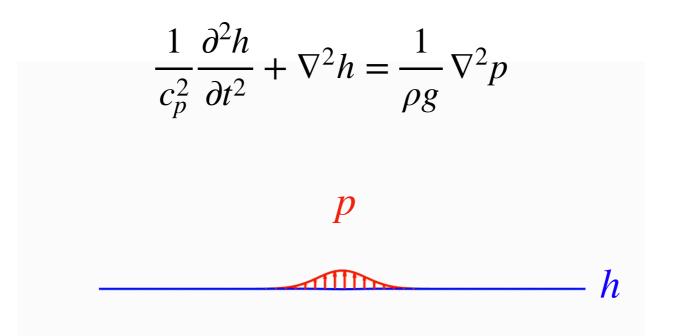




Dimensionless parameters:

$$\alpha = L/W, \quad \beta = L/D, \quad \phi, \quad \theta, \quad Fr_{\omega}, \quad Fr$$

Minimal (non-dispersive) model



I.Apply a Lorentz transformation:

$$\gamma = (1 - U^2/c_p^2)^{-1/2}$$

$$\tilde{X} = \gamma(x - Ut)$$
$$\tilde{y} = y$$
$$\tilde{t} = \gamma(t - Ux/c_p^2)$$



I.Apply a Lorentz transformation:

$$\gamma = (1 - U^2/c_p^2)^{-1/2}$$

$$\begin{split} \tilde{X} &= \gamma(x - Ut) \\ \tilde{y} &= y \\ \tilde{t} &= \gamma(t - Ux/c_p^2) \end{split}$$



Helmholtz Equation $(\tilde{\nabla}^2 \bar{h} + k^2 \bar{h} = - \tilde{\nabla}^2 \bar{p} / \rho g)$

2. Seek a solution:

$$h = \operatorname{Im}\left\{\bar{h}e^{i\omega t}\right\}$$

I.Apply a Lorentz transformation:

$$\gamma = (1 - U^2/c_p^2)^{-1/2}$$

$$\begin{split} \tilde{X} &= \gamma(x - Ut) \\ \tilde{y} &= y \\ \tilde{t} &= \gamma(t - Ux/c_p^2) \end{split}$$



3. Method of Green's functions:

-5

0

2

-2

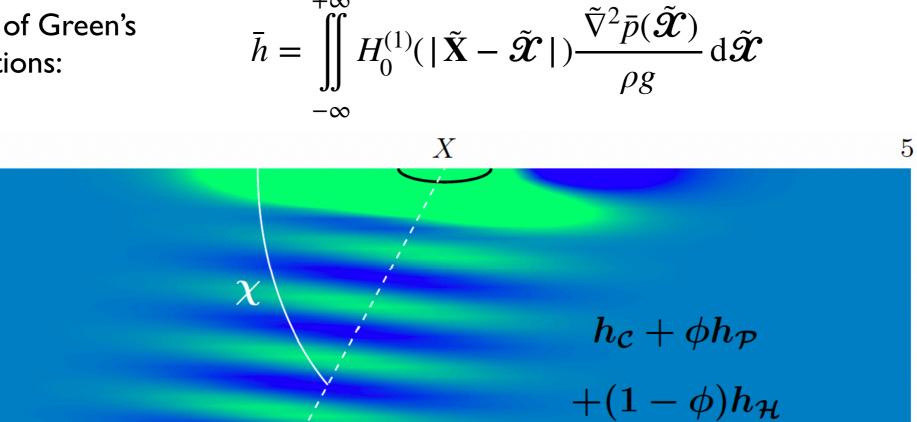
 -5×10^{-3}

2. Seek a solution:

$$h = \operatorname{Im}\left\{\bar{h}e^{i\omega t}\right\}$$

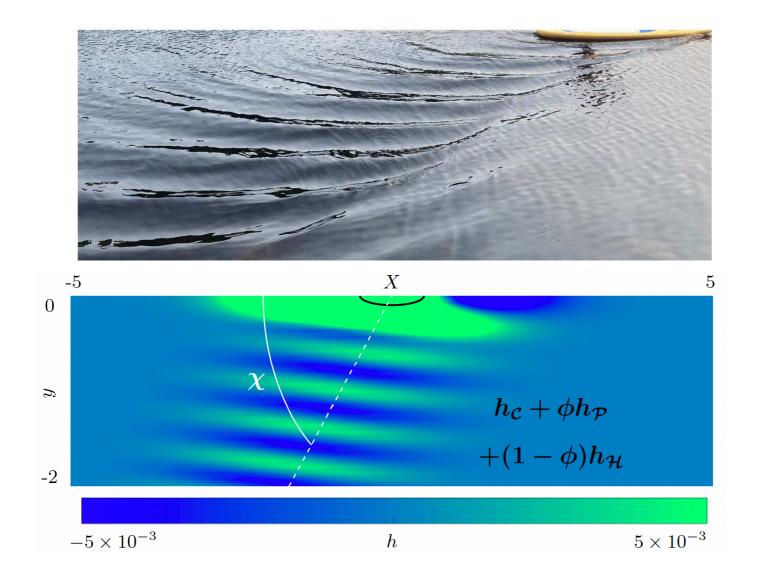
Helmholtz Equation $(\,\tilde{\nabla}^2\bar{h} + k^2\bar{h} = -\,\tilde{\nabla}^2\bar{p}/\rho g)$

 5×10^{-3}



h

COMPARISON WITH DATA



THRUST-DRAG BALANCE

$$F = \iint p \frac{\partial h}{\partial X} dS = \frac{1}{2} \rho C_D U^2 A$$

$$\implies U \approx 1.5 \text{ m/s}$$
WAKE ANGLE
 $\chi = \tan^{-1} 1/\text{Ma} \approx 51^\circ$

OTHER FINDINGS:

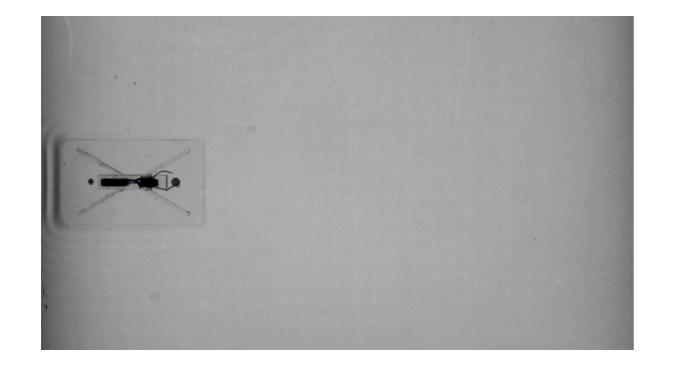
Must have heaving **and** pitching to generate thrust

Optimum parameters: $\phi = 1/2, \quad \theta = \pi/2$

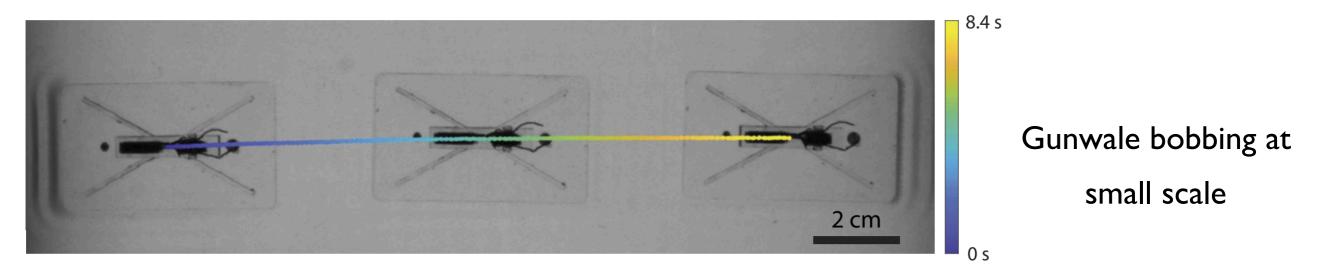
GPB, et al, PRF (2022) + Nature (Research Highlight)

SURFERBOT

OSCILLATING, FLOATING RAFT WITH ASYMMETRIC WEIGHT





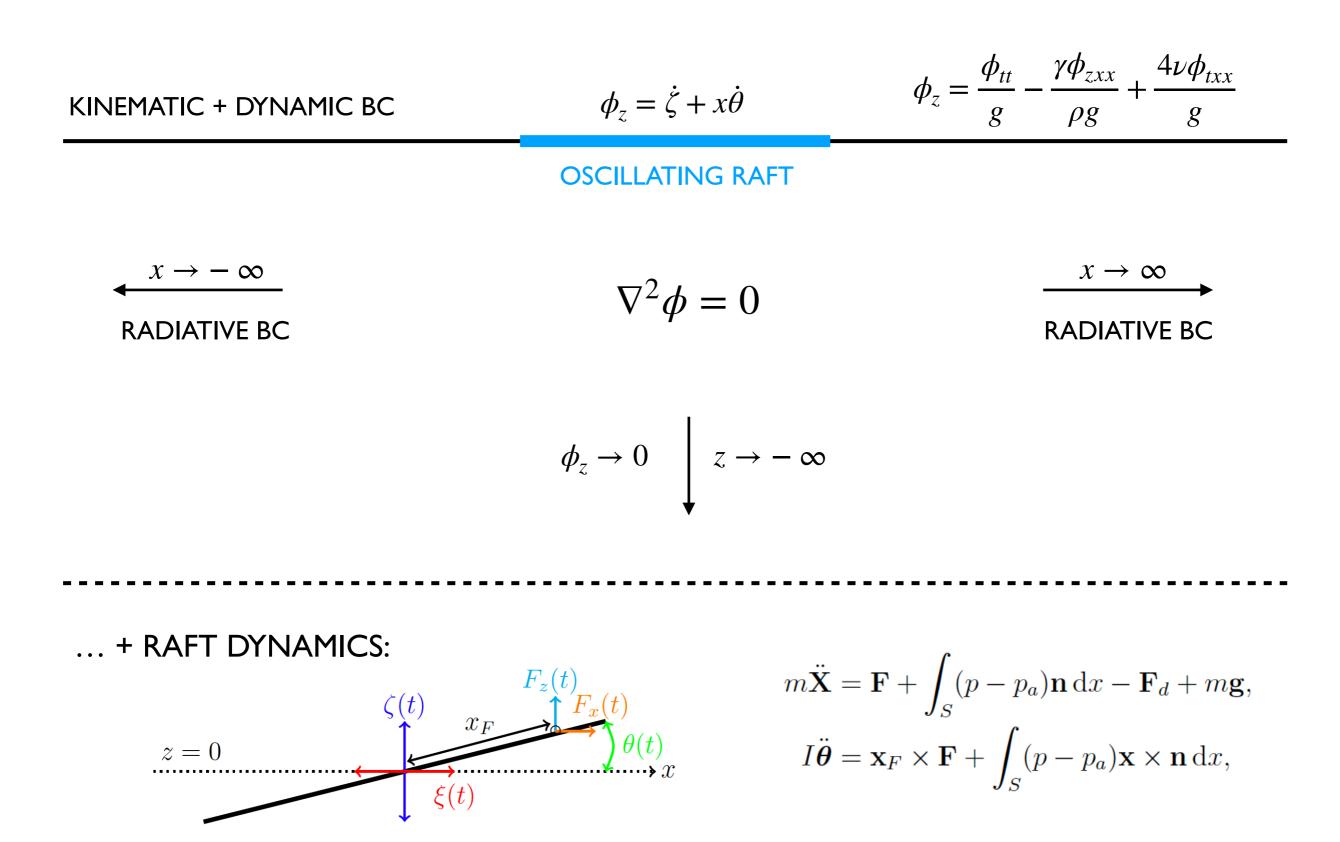


Rhee, Hunt, Thomson & Harris. (2022)

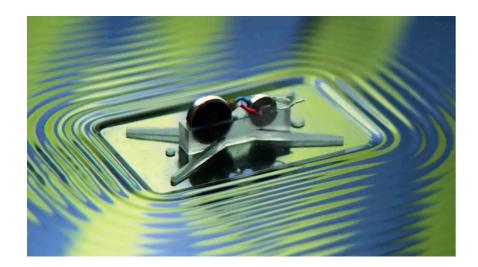
LINEAR DISPERSIVE MODEL FOR WAVE-DRIVEN PROPULSION

KINEMATIC + DYNAMIC BC	$\phi_z = \dot{\zeta} + x\dot{\theta}$	$\phi_z = \frac{\phi_{tt}}{g} - \frac{\gamma \phi_{zxx}}{\rho g} + \frac{4\nu \phi_{txx}}{g}$
	OSCILLATING RAFT	
$\begin{array}{c} x \rightarrow -\infty \\ \hline \\ \textbf{RADIATIVE BC} \end{array}$	$\nabla^2 \phi = 0$	$\xrightarrow{x \to \infty}$ RADIATIVE BC
	$\phi_z \to 0 \int z \to -\infty$	

LINEAR DISPERSIVE MODEL FOR WAVE-DRIVEN PROPULSION



SURFERBOT DATA



0

0.2

0.4

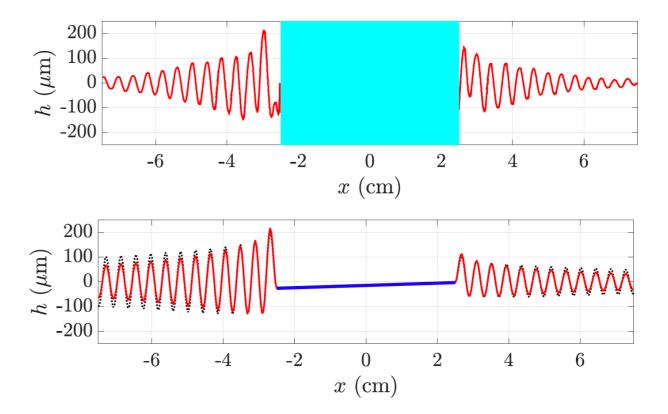
x (mm)

0.6

0.8

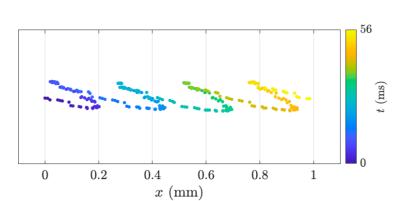
1



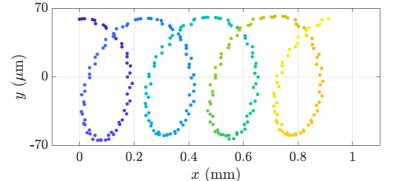


FRONT POSITION



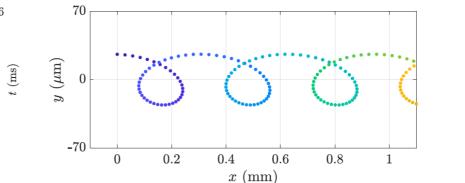


56



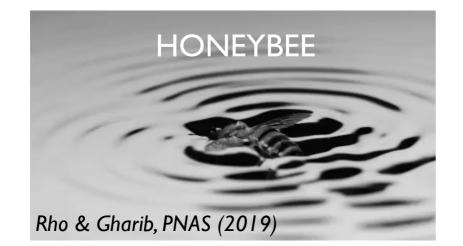
EXPERIMENT

THEORY





WAVE-DRIVEN PROPULSION ACROSS SCALES



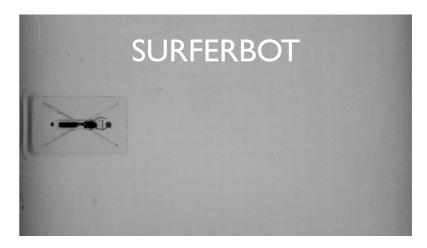
Fr = 0.1	$Fr_{\omega} = 0.07$
$Re = 10^2$	We = 0.1



$$Fr = 0.7$$

 $Re = 10^4$ $We = 10^2$

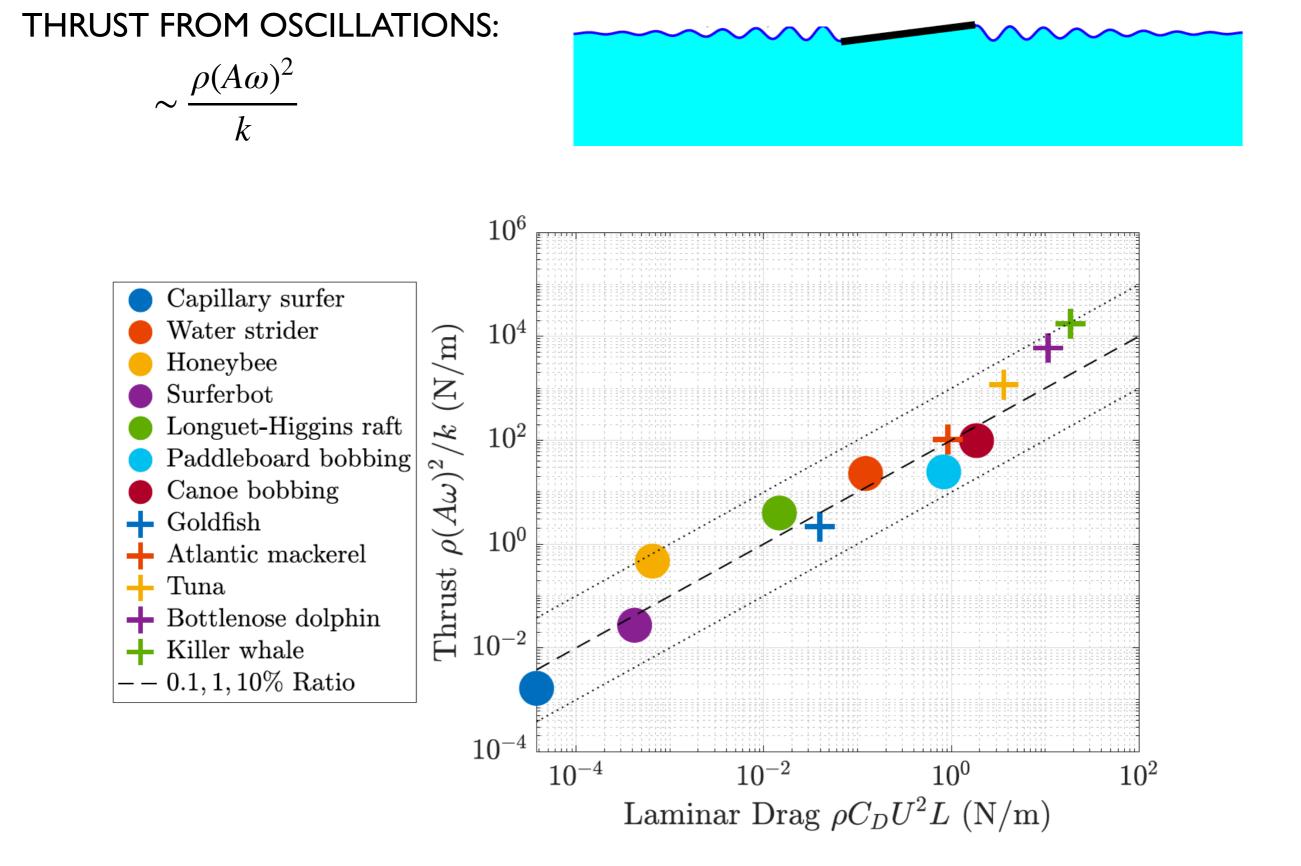
 $\operatorname{Re} = UL/\nu$ $\operatorname{Fr} = U/\sqrt{gL}$



Fr = 0.03 Fr_{ω} = 0.03 Re = 10³ We = 0.3

$$Fr = 0.2$$
 $Fr_{\omega} = 0.2$
 $Re = 10^6$
 $We = 10^5$

 $\operatorname{Fr}_{\omega} = \omega^{-1} \sqrt{g/L}$ We $= \rho U^2 L/\gamma$



GPB, Devauchelle & Thomson (in preparation)

QUESTIONS?

11

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